

# *High Level Waste Tank Seismic/Structural Analysis*

WSRC Structural Mechanics  
May 13, 2008

# Introduction

- Analysis performed using guidance of:

Tank Seismic Experts Panel (TSEP); Seismic Design and Evaluation Guidelines for DOE High Level Waste Storage Tanks (BNL 52361)

- Stress acceptance criteria:

Concrete vault: ACI 349

Steel tanks: ASME Section III Subsection NC-3200

# Introduction

- Tank analysis divided into two independent elements:

Concrete vault

Steel tank

- Analysis concentrated on Type III tanks – results used to guide approach on other tanks

# Vault Structural Analysis

- Evaluated for all operating/normal loads:

- Dead and live including loads on tank tops

- Fluid

- Earth pressure

- Annulus and tank internal pressures or vacuum

- Thermal

- Static settlement

# Vault Structural Analysis

## Natural Phenomena Hazards

- Seismic:

  - Tank fill height and viscosity variations

  - Fluid hydrodynamic behavior (slosh)

  - Soil-structural interaction (SSI)

- SSI required numerous variation:

  - Tank with top at grade

  - Tank in a hill

  - Tank to tank interaction

# Vault Structural Analysis – Plan & Cross Section

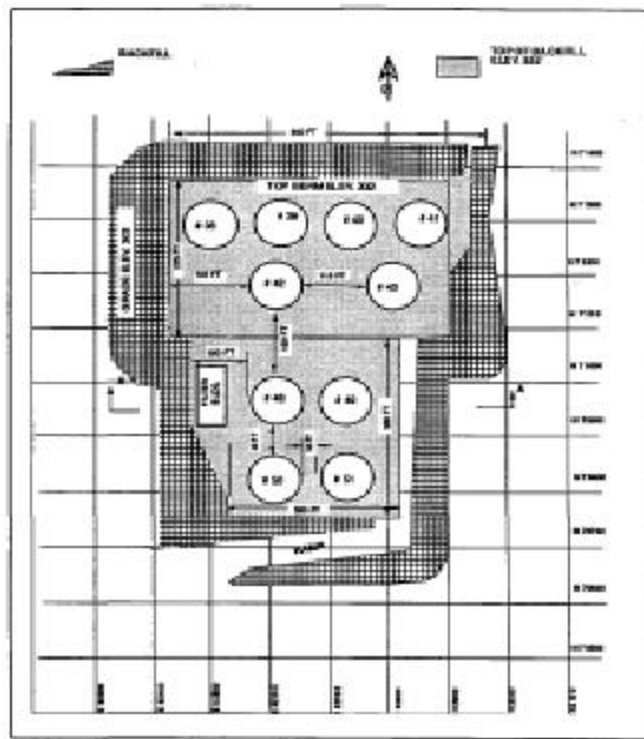


Figure 1.1 H-Area ITP Facility

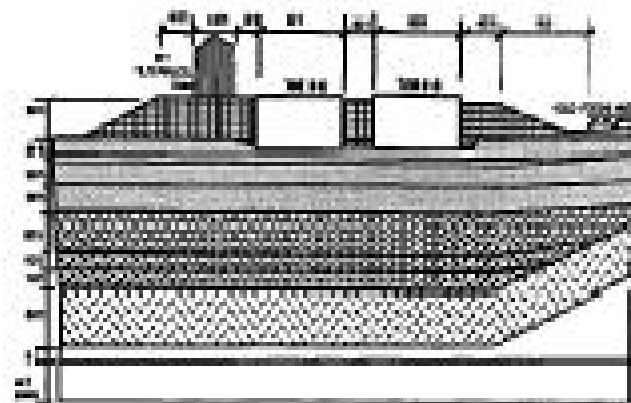
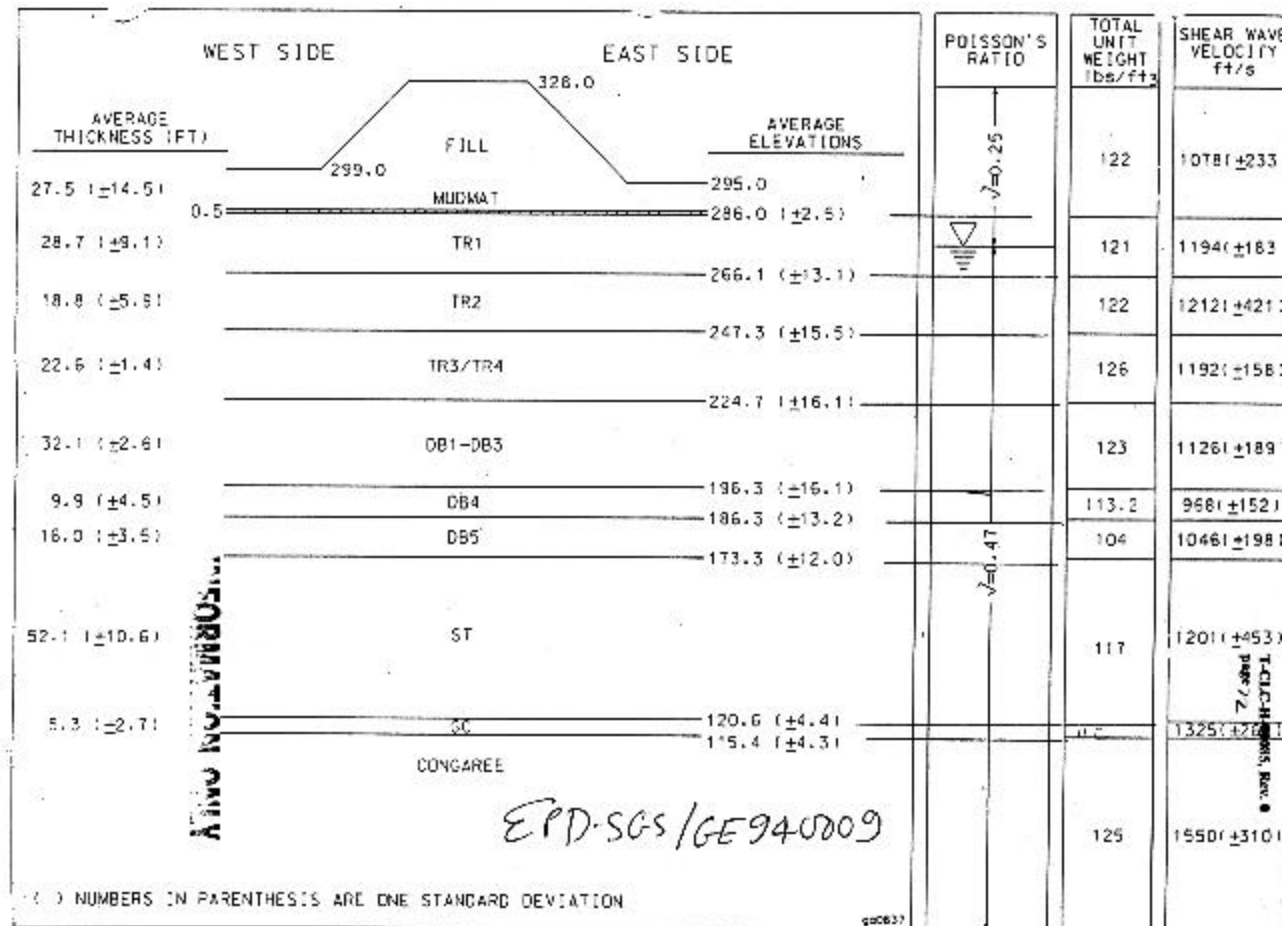
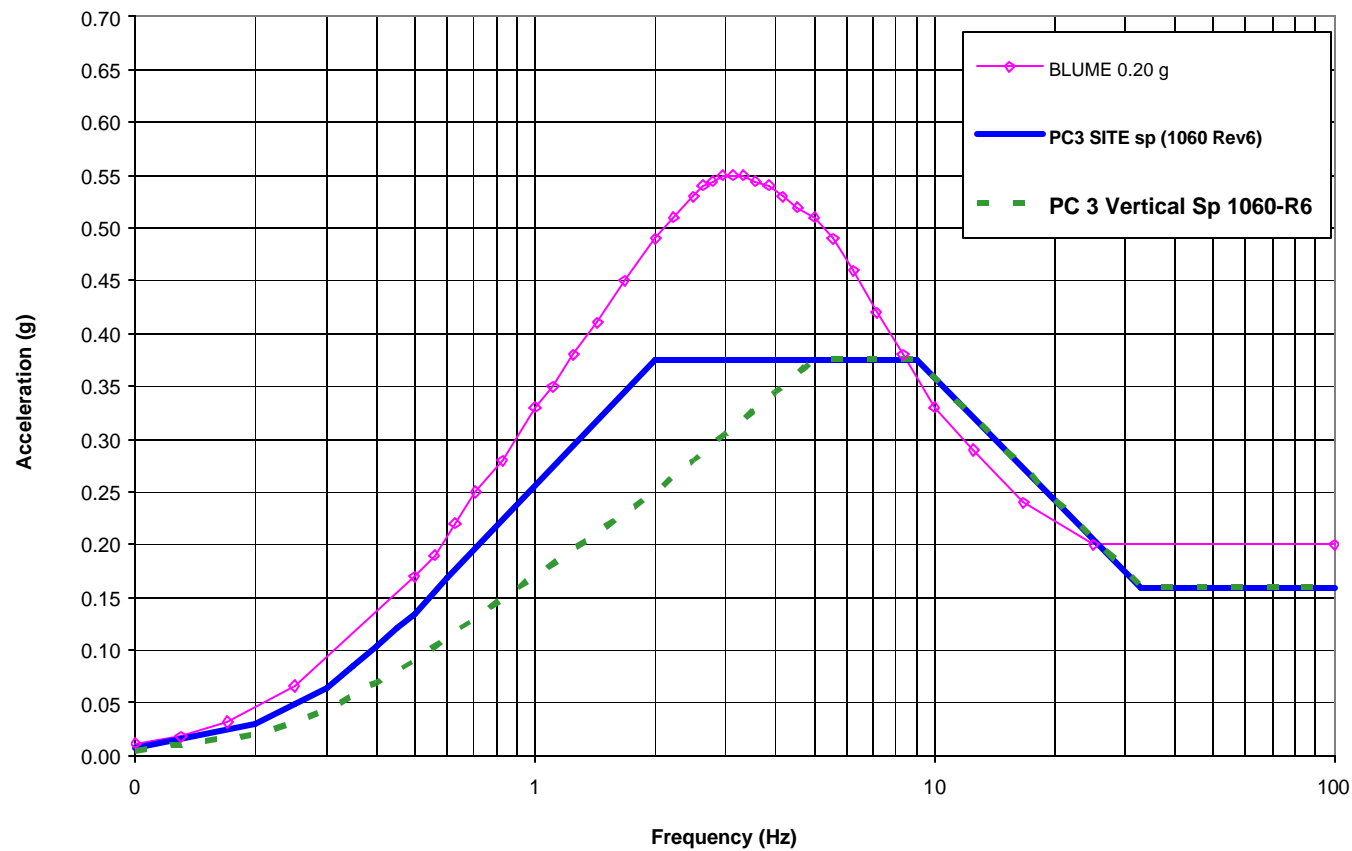


Figure 1.2 H-Area ITP Facility Section A-A

# Vault Structural Analysis - Soil Profile



# Vault Structural Analysis - BLUME vs. PC-3 Site Specific





# Vault Structural Analysis - SASSI 3D Model

The stiffness of the secondary liner  
is included in concrete wall thickness.

Reinforced concrete

$f'_c = 3000 \text{ psi}$

Young's Modulus,  $E_c = 450,000 \text{ ksf}$

Reinforcing Steel  $f_y = 60 \text{ ksi}$

Poisson's ratio = 0.2

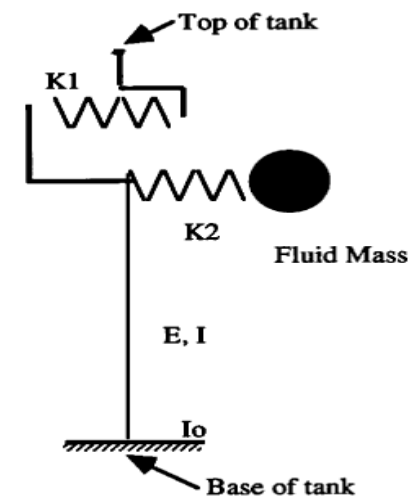
Density = .15 kcf

The secondary liner properties are:

$f_y = 38 \text{ ksi}$

$E = 29,000 \text{ psi} = 4,176,000 \text{ ksf}$

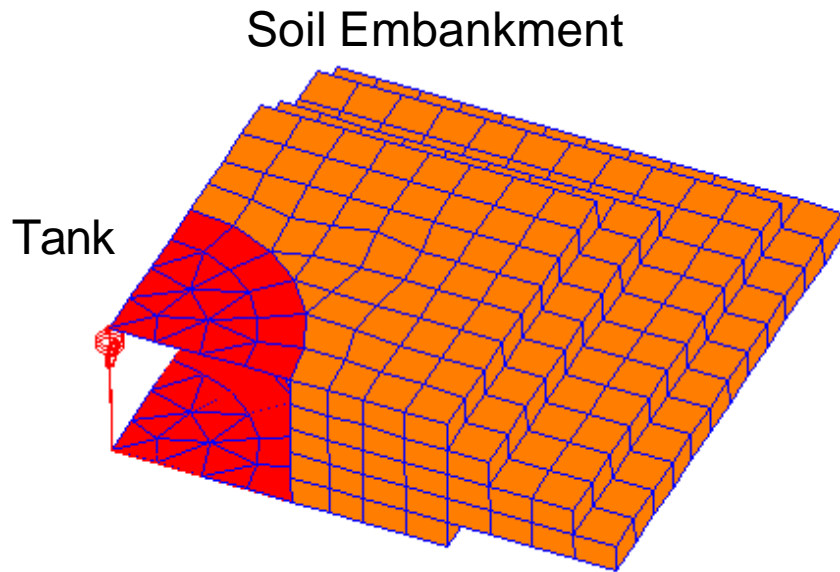
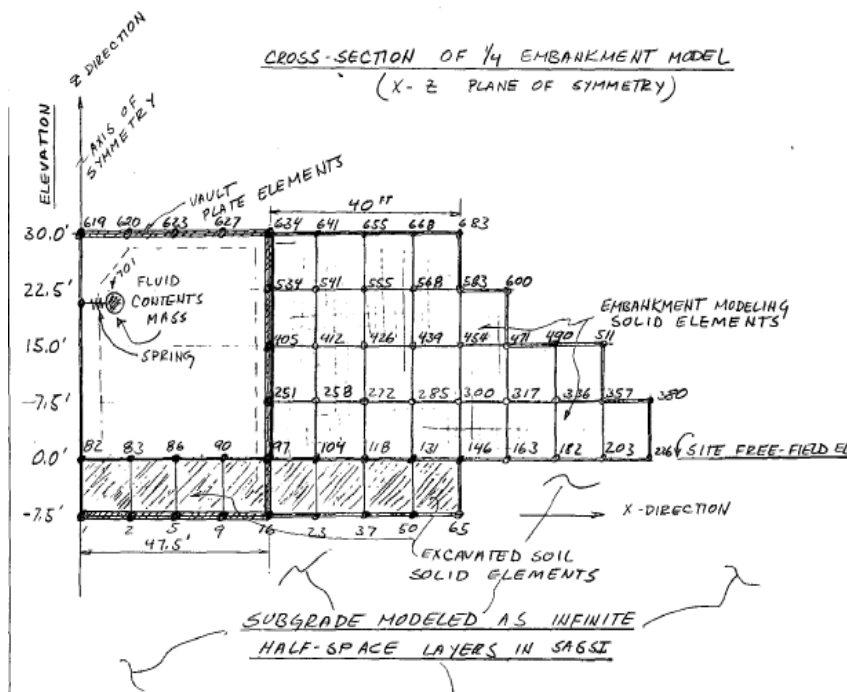
$n = E/E_c = 9.3$



K1	=	1,040,000 k/ft
K2	=	520,000 k/ft
E	=	4,250,000 ksf
I	=	3208 ft <sup>4</sup>
Fluid Weight	=	10,950 k
Io	=	1,246,040 (mass moment of inertia)

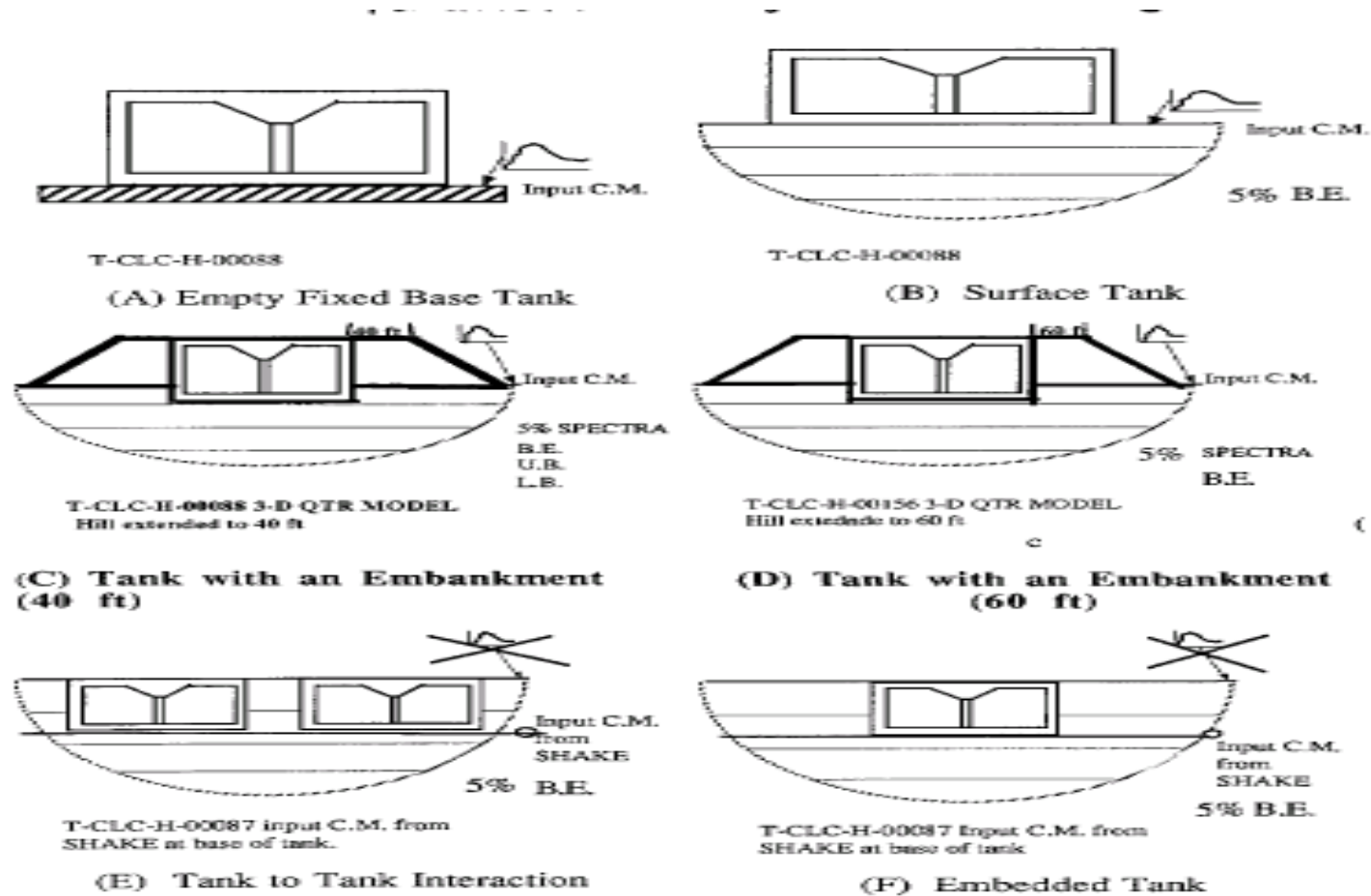
Stick Representation of Fluid  
using BNL 52361

# Vault Structural Analysis - 3-D Finite Element model of Tank and Soil Embankment



## SASSI Model

# Vault Structural Analysis - SSI Analysis



## Vault Structural Analysis – Seismic Analysis Conclusions

- Normal operating loads met code allowable
- Tank top was marginal – tank top loads (additions/removals) are controlled under LWO program
- SSI had negligible effect – consequently analysis not performed for Type I and II tanks

# Vault/Tank Structural Analysis - Differential Settlement

- Post seismic differential settlement resulting from:

Partial liquefaction

Collapse of subsurface voids

Subsidence of soft zones

- Postulated as a surface subsidence of circular pattern of 95' diameter

Design basis depth 1.75"

Due to uncertainty: beyond design basis depth 3"

- Concrete vault and steel tanks evaluated separately using FEA (ABAQUS)

# Vault/Tank Structural Analysis - Differential Settlement

## Center Settlement Profile

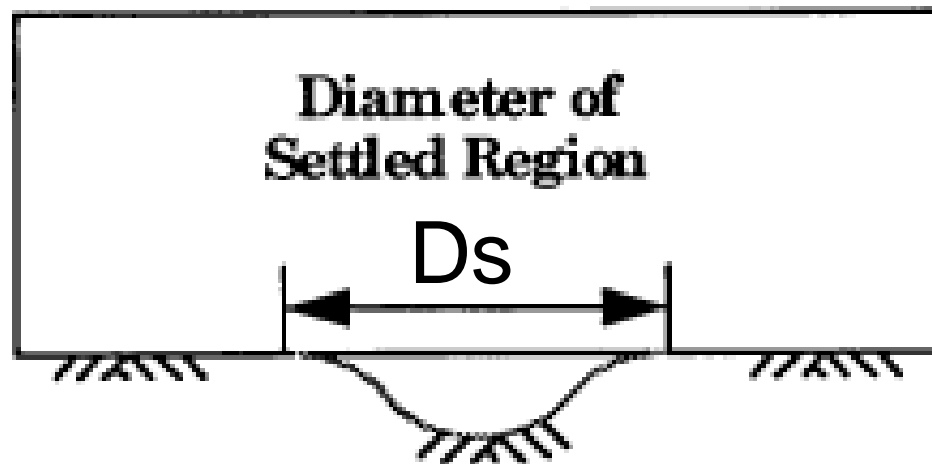


Figure 4.41

# Vault/Tank Structural Analysis - Differential Settlement

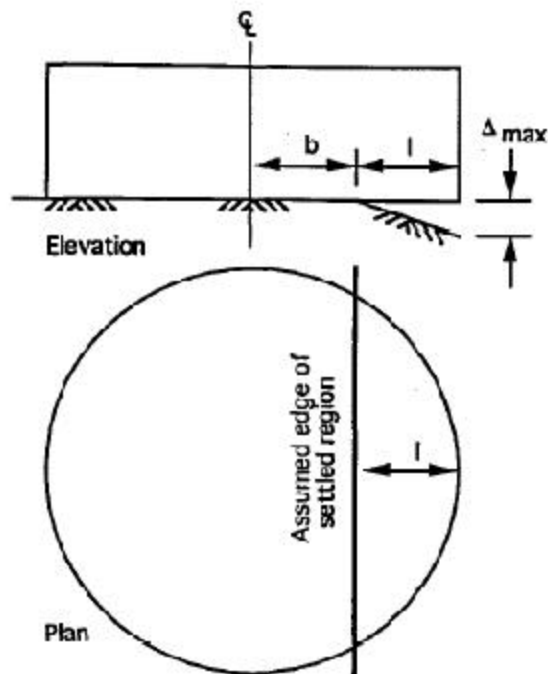


Figure 4.46 Edge Settlement Profile

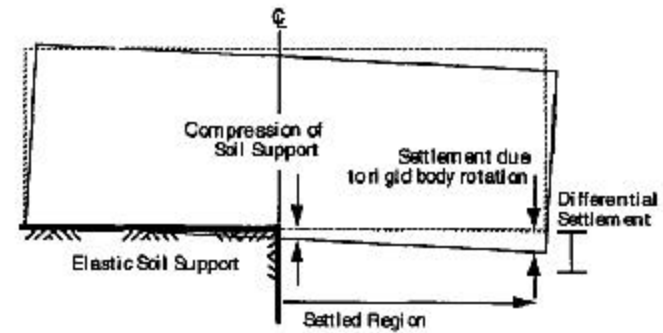


Figure 4.47 Rigid Body Rotation of the Vault due to Compression of Soil

# Vault/Tank Structural Analysis - Differential Settlement

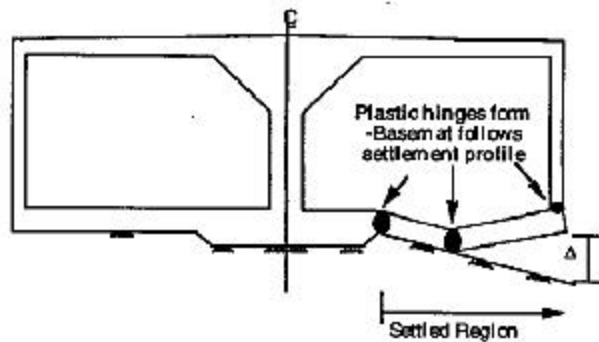


Figure 4.48 Cross Section Through Vault with Edge Settlement Profile and Possible Basemat Collapse Mechanism

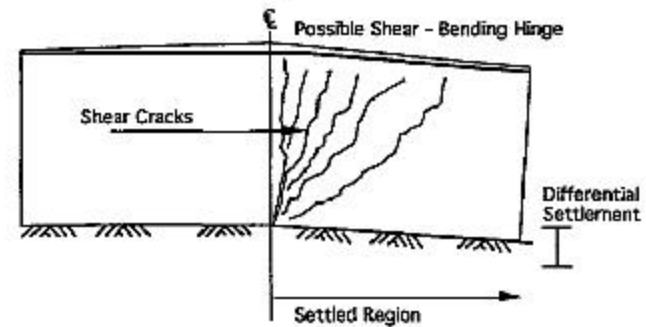
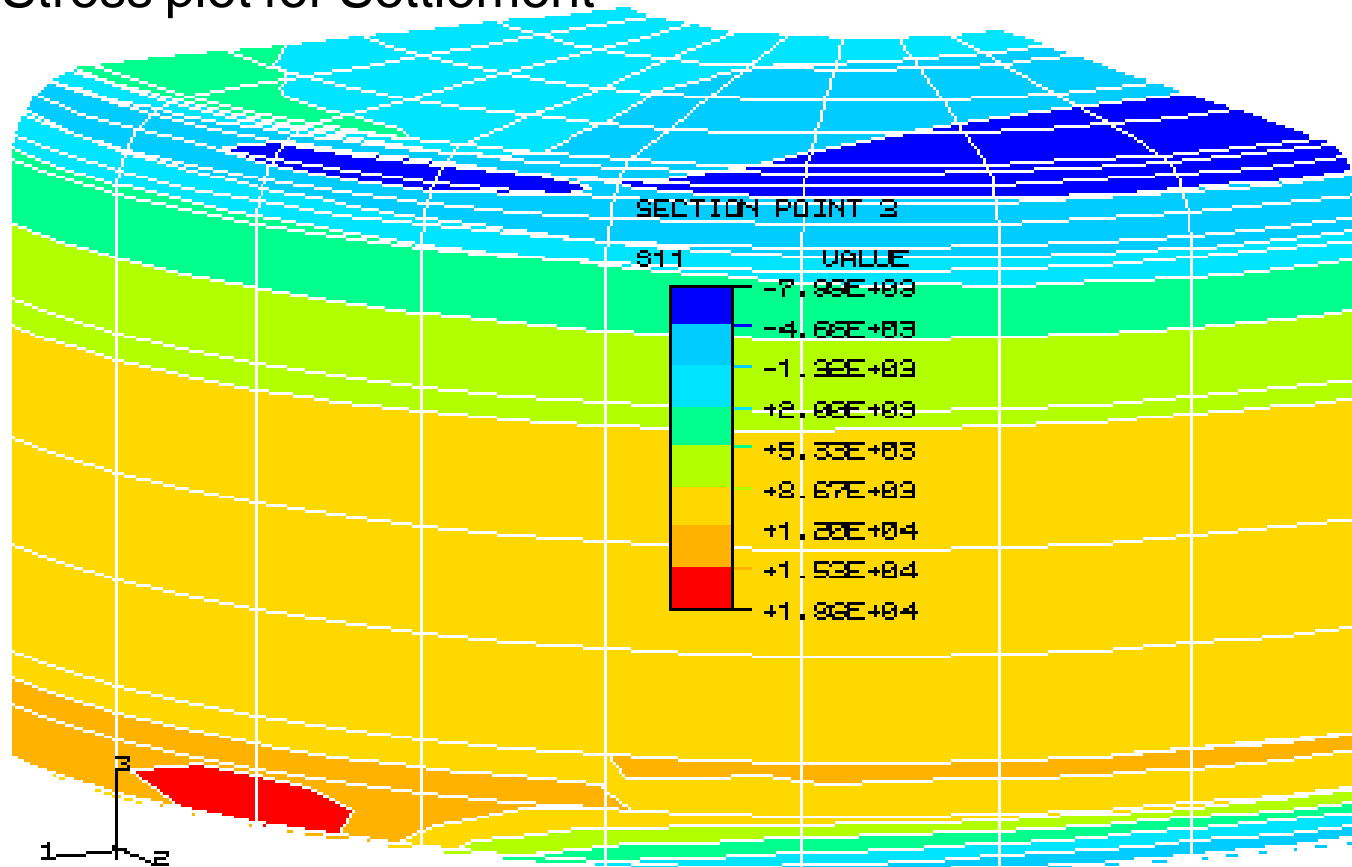


Figure 4.49 Vault Wall Shear and Bending Mechanism for the Edge Settlement Profile



# Vault/Tank Structural Analysis - Differential Settlement

Tank Stress plot for Settlement



# Tank Structural Analysis - Differential Settlement Results

**Table 4.21**  
**Steel Tank Allowable Soil Settlement for**  
**ITP Tanks and Type III Tanks**

	<b>Center Settlement</b>	<b>Edge Settlement w/ Vault Wall Failure</b>	<b>Edge Settlement w/o Vault Wall Failure</b>
<b>Vault Failure Mechanism</b>	<b>Base Slab and Roof Slab Failure</b>	<b>Failure of Base Slab, Roof Slab, and Vault Wall @ Vault Edge</b>	<b>Base Slab Failure Only</b>
<b>Figure No.</b>	<b>4.41, 4.44</b>	<b>4.42, 4.45</b>	<b>4.42, 4.48</b>
<b>Tank Deformations</b>	<b>14. in</b>	<b>1. in</b>	<b>6.6 in</b>
<b>Rigid Body Rotation</b>	<b>0. in</b>	<b>3.7 in</b>	<b>5.3 in</b>
<b>Maximum Allowable Differential Settlement</b>	<b>14. in</b>	<b>4.7 in</b>	<b>12. in</b>
<b>Stress Intensity Margin</b>	<b>0.0</b>	<b>1.4</b>	<b>1.4</b>
<b>Buckling Margin</b>	<b>0.43</b>	<b>-0.17</b>	<b>-0.17</b>

# Vault Structural Analysis - Differential Settlement Results

Concrete Vault “allowable” settlement

- Tanks 35 to 43 and 48 to 51: 5.1”
- Tanks 29 to 32: 5.5”
- Collapse occurs at settlement > 23”

# Tank Analysis

FEA (ABAQUS)

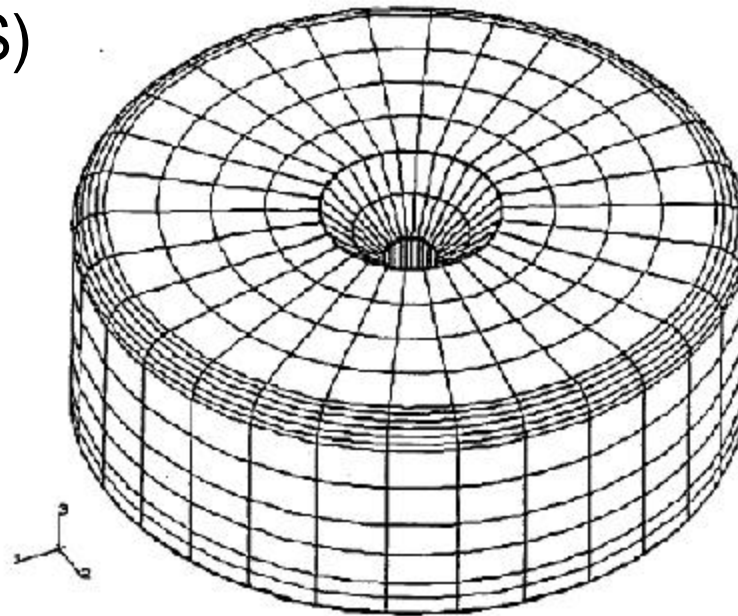


Figure 4.51  
Finite Element Analysis Model

# Tank Analysis

Determine Stresses from Normal Loads:

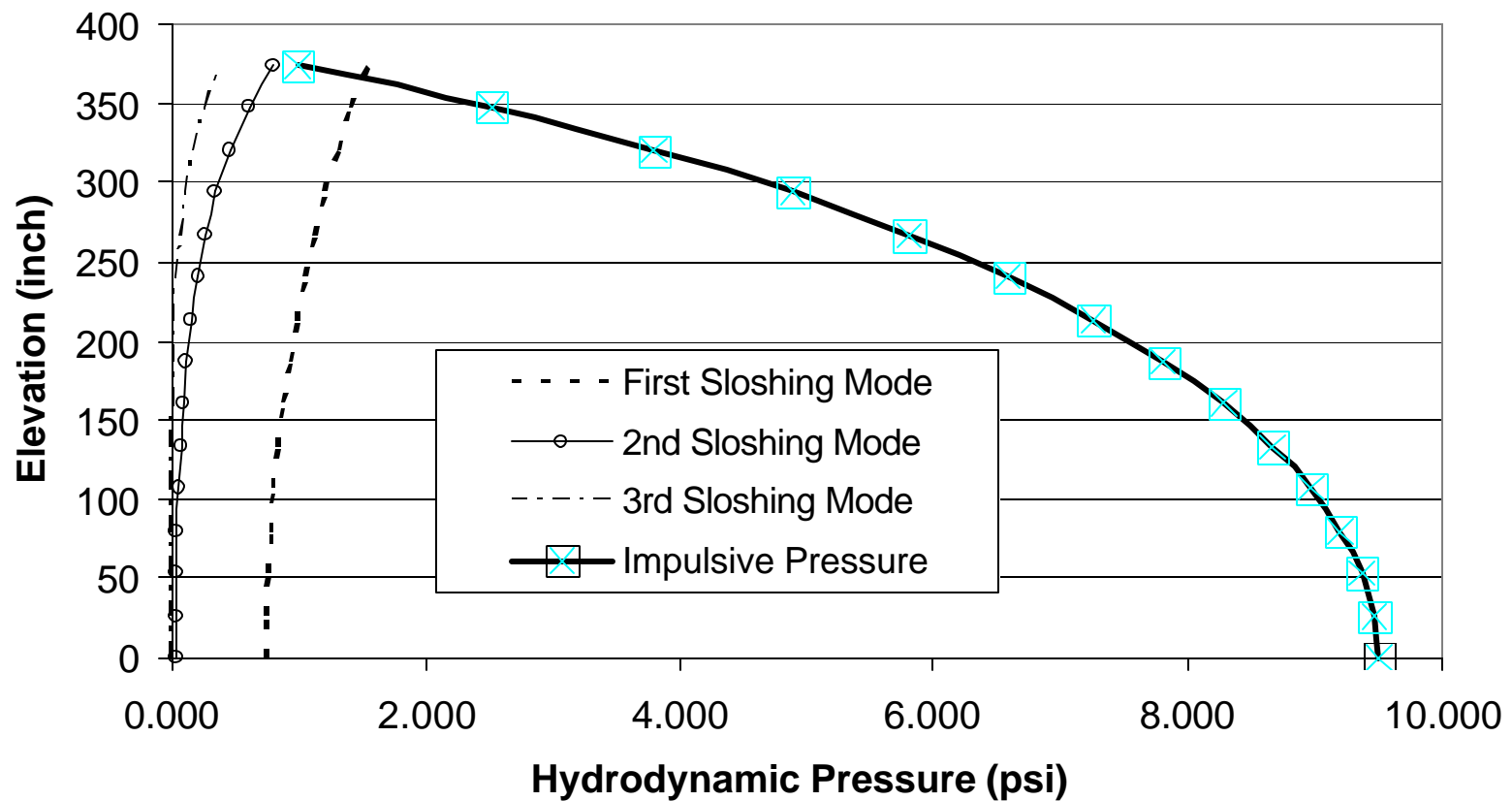
- Hydrostatic Fluid Pressure
- Annulus Vacuum/Pressure
- Tank Ventilation Pressures
- Jet impingement Loads
- Thermal Stress
- Salt loads on Tank wall

# Tank Analysis

## PC-3 Seismic Loads

- Horizontal Convective Mode
- Horizontal Impulsive Mode
- Tank Top Contact - Constrained Fluid Response
- Tank Top Contact - Fluid Impact
- Vertical Response Mode

# Tank Analysis



# Tank Analysis

- Compilation of FEA Results confirm that the tank stress condition can be computed, within 5%, by

$$Pr/t$$

- where:  
P = total Pressure contribution from fluid pressure, seismic pressures, and annulus pressures, (all hand calcs).  
r= tank radius  
t= wall thickness



# Tank Analysis

Additional work that evolved from baseline analysis:

- Cooling coils loading
- Bottom pitting
- Dented walls
- Annulus vacuum
- Wall thinning

# Tank Analysis – Wall Thinning Evaluation

